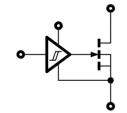




650 V GaNFast™ Power IC

FF



QFN 5 x 6 mm

Simplified schematic

1. Features

GaNFast™ Power IC

- · Monolithically-integrated gate drive
- Wide logic input range with hysteresis
- 5 V / 15 V input-compatible
- Wide V_{CC} range (10 to 30 V)
- Programmable turn-on dV/dt
- 200 V/ns dV/dt immunity
- · 650 V eMode GaN FET
- Low 120 mΩ resistance
- · Zero reverse recovery charge
- · 2 MHz operation

Small, low-profile SMT QFN

- 5 x 6 mm footprint, 0.85 mm profile
- · Minimized package inductance

Environmental

· RoHS, Pb-free, REACH-compliant

2. Description

The NV6117 is a 650 V GaNFast™ power IC, optimized for high frequency, soft-switching topologies.

Monolithic integration of FET, drive and logic creates an easy-to-use 'digital-in, power-out' high-performance powertrain building block, enabling designers to create the fastest, smallest, most efficient integrated powertrain in the world.

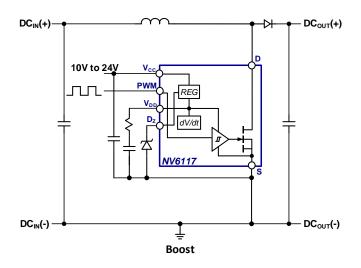
The highest dV/dt immunity, high-speed integrated drive and industry-standard low-profile, low-inductance, 5 x 6 mm SMT QFN package allow designers to exploit Navitas GaN technology with simple, quick, dependable solutions for breakthrough power density and efficiency.

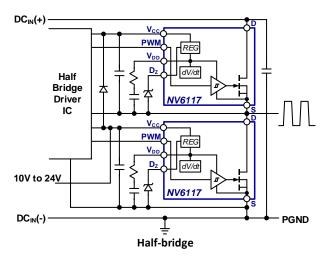
Navitas' GaNFast™ power ICs extend the capabilities of traditional topologies such as flyback, half-bridge, resonant, etc. to MHz+ and enable the commercial introduction of breakthrough designs.

3. Topologies / Applications

- · AC-DC, DC-DC, DC-AC
- · Buck, boost, half bridge, full bridge
- · Active Clamp Flyback, LLC resonant, Class D
- · Mobile fast-chargers, adapters
- · Notebook adaptors
- LED lighting, solar micro-inverters
- TV / monitor, wireless power
- · Server, telecom & networking SMPS

4. Typical Application Circuits







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6. Specifications

6.1. Absolute Maximum Ratings(1)

(with respect to Source (pad) unless noted)

SYMBOL	PARAMETER	MAX	UNITS
V _{DS}	Drain-to-Source Voltage	-7 to +650	V
V _{TDS}	Transient Drain-to-Source Voltage ⁽²⁾		V
V _{cc}	V _{CC} Supply Voltage		V
V _{PWM}	PWM Input Pin Voltage	-3 to +30	V
V _{DZ}	V _{DZ} V _{DD} Setting Pin Voltage		V
V _{DD}	V _{DD} Drive Supply Voltage		V
I _D	I _D Continuous Drain Current (@ T _C = 100°C)		А
I _D PULSE	I _D PULSE Pulsed Drain Current (10 μs @ T _J = 25°C)		Α
I _D PULSE	I _D PULSE Pulsed Drain Current (10 μs @ T _J = 125°C)		А
dV/dt	dV/dt Slew Rate on Drain-to-Source		V/ns
T_{J}	T _J Operating Junction Temperature		°C
T _{STOR}	Storage Temperature	-55 to 150	°C

⁽¹⁾ Absolute maximum ratings are stress ratings; devices subjected to stresses beyond these ratings may cause permanent damage.

6.2. Recommended Operating Conditions(3)

SYMBOL	PARAMETER	MIN	TYP	MAX	UNITS
V _{DZ}	Drive Supply Set Zener Voltage ⁽⁴⁾	5.8	6.2	6.6	V
V_{DD}	Drive Supply Voltage	5.5		7.0	V
I _{DD_EXT}	I _{DD_EXT} Regulator External Load Current			3.0	mA
R _{DD}	Gate Drive Turn-On Current Set Resistance ⁽⁵⁾		25	200	Ω
V _{PWM}	PWM Input Pin Voltage		5	Min. of (V _{cc} or 20)	V
V _{DS}	Drain-to-Source Voltage			520	V
V _{cc}	Supply Voltage	10		24	V
TJ	Operating Junction Temperature	-40		125	°C

⁽³⁾ Exposure to conditions beyond maximum recommended operating conditions for extended periods of time may affect device reliability.

^{(2) &}lt; 1 μ S. V_{TDS} is intended for surge rating during non-repetitive events (for example start-up, line interruption).

⁽⁴⁾ Use of zener diode other than 6.2 V is not recommended. See Table I for recommended part numbers of 6.2 V zener diodes.

⁽⁵⁾ R_{DD} resistor <u>must be used</u>. Minimum 10 Ohm to ensure application and device robustness.





6.3. ESD Ratings

SYMBOL	PARAMETER	MAX	UNITS
НВМ	Human Body Model (per JS-001-2014)	1,000	V
CDM	Charged Device Model (per JS-002-2014)	1,000	V

6.4. Thermal Resistance

SYMBOL	PARAMETER	TYP	UNITS
R _{eJC} (6)	Junction-to-Case	1.8	°C/W
R _{eJA} (6)	Junction-to-Ambient	50	°C/W

⁽⁶⁾ R_{e} measured on DUT mounted on 1 square inch 2 oz Cu (FR4 PCB)





6.5. Electrical Characteristics

Typical conditions: $V_{DS} = 400 \text{ V}$, $V_{CC} = 15 \text{ V}$, $V_{DZ} = 6.2 \text{ V}$, $F_{SW} = 1 \text{ MHz}$, $T_{AMB} = 25 \, ^{\circ}\text{C}$, $I_{D} = 6 \text{ A}$, $R_{DD} = 10 \, \Omega$ (or specified)

SYMBOL	PARAMETER	MIN	TYP	MAX	UNITS	CONDITIONS
		V _{cc} Sup	ply Chara	acteristic	S	
I _{QCC}	V _{cc} Quiescent Current		0.85	1.5	mA	V _{PWM} = 0 V
I QCC-SW	V _{cc} Operating Current		2.85		mA	F _{SW} = 1 MHz, V _{DS} = Open
	Low	-Side Log	gic Input	Characte	ristics	
$V_{_{\mathrm{PWMH}}}$	Input Logic High Threshold (rising edge)			4	V	
$V_{_{PWML}}$	Input Logic Low Threshold (falling edge)	1			٧	
V _{I-HYS}	Input Logic Hysteresis		0.5		V	
T _{on}	Turn-on Propagation Delay		11		ns	Fig.1, Fig.2
T _{OFF}	Turn-off Propagation Delay		9		ns	Fig.1, Fig.2
$T_{_{R}}$	Drain rise time		6		ns	Fig.1, Fig.2
T _F	Drain fall time		3		ns	Fig.1, Fig.2
Switching Characteristics						
F _{sw}	Switching Frequency			2	MHz	
t _{PW}	Pulse width	0.02		1000	μs	
		GaN FE	ET Chara	cteristics		
l _{DSS}	Drain-Source Leakage Current		0.3	25	μΑ	$V_{DS} = 650 \text{ V}, V_{PWM} = 0 \text{ V}$
l _{DSS}	Drain-Source Leakage Current		10		μΑ	$V_{DS} = 650 \text{ V}, V_{PWM} = 0 \text{ V}, T_{C} = 125 ^{\circ}\text{C}$
R _{DS(ON)}	Drain-Source Resistance		120	170	mΩ	$V_{PWM} = 6 \text{ V}, I_D = 6 \text{ A}$
V _{SD}	Source-Drain Reverse Voltage		3.2	5	٧	$V_{PWM} = 0 \text{ V}, I_{SD} = 6 \text{ A}$
$Q_{_{\mathrm{OSS}}}$	Output Charge		27		nC	$V_{DS} = 400 \text{ V}, V_{PWM} = 0 \text{ V}$
$Q_{_{RR}}$	Reverse Recovery Charge		0		nC	
C _{oss}	Output Capacitance		27		pF	$V_{DS} = 400 \text{ V}, V_{PWM} = 0 \text{ V}$
C _{O(er)} (7)	Effective Output Capacitance, Energy Related		41		pF	V _{DS} = 400 V, V _{PWM} = 0 V
C _{O(tr)} (8)	Effective Output Capacitance, Time Related		67		pF	$V_{DS} = 400 \text{ V}, V_{PWM} = 0 \text{ V}$

⁽⁷⁾ $C_{O(er)}$ is a fixed capacitance that gives the same stored energy as C_{OSS} while V_{DS} is rising from 0 to 400 V

⁽⁸⁾ $C_{\text{O(tr)}}$ is a fixed capacitance that gives the same charging time as C_{OSS} while V_{DS} is rising from 0 to 400 V





6.6. Switching Waveforms

(T_C = 25 °C unless otherwise specified)

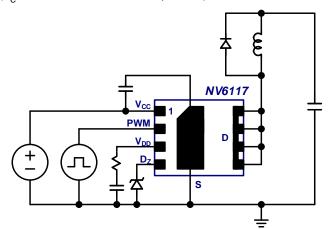


Fig.1. Inductive switching circuit

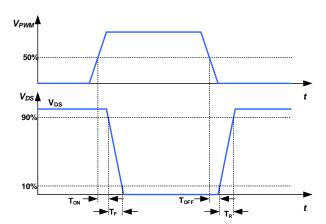


Fig.2. Propagation delay and rise/fall time definitions





6.7. Characteristic Graphs

(GaN FET, T_C = 25 °C unless otherwise specified)

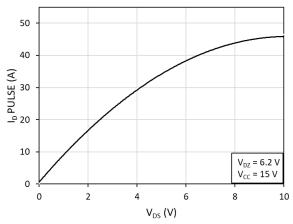


Fig.3. Pulsed Drain current (I_D PULSE) vs. drain-to-source voltage (V_{DS}) at T = 25 °C

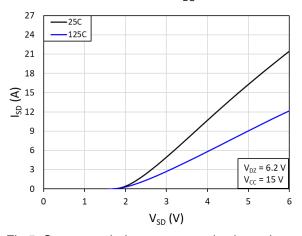


Fig.5. Source-to-drain reverse conduction voltage

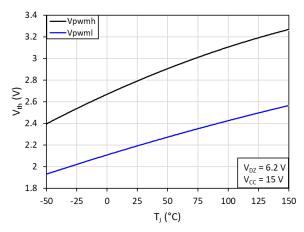


Fig.7. V_{PWMH} and V_{PWML} vs. junction temperature(T_{J})

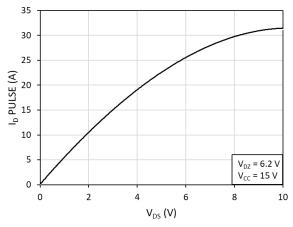


Fig.4. Pulsed Drain current (I_D PULSE) vs. drain-to-source voltage (V_{DS}) at T = 125 °C

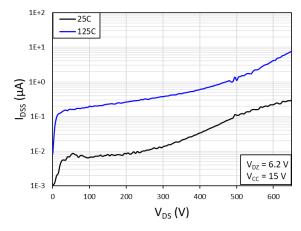


Fig.6. Drain-to-source leakage current (I_{DSS}) vs. drain-to-source voltage (V_{DS})

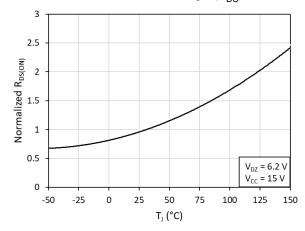


Fig.8. Normalized on-resistance $(R_{DS(ON)})$ vs. junction temperature (T_J)





Characteristic Graphs (Cont.)

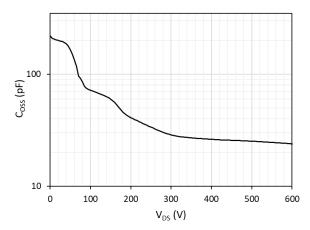


Fig.9. Output capacitance (C_{OSS}) vs. drain-to-source voltage (V_{DS})

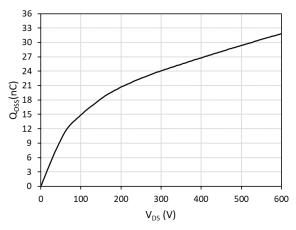


Fig.11. Charge stored in output capacitance (Q_{OSS}) vs. drain-to-source voltage (V_{DS})

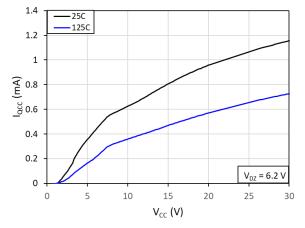


Fig.13. V_{CC} quiescent current (I_{QCC}) vs. supply voltage (V_{CC})

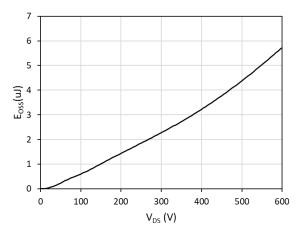


Fig.10. Energy stored in output capacitance (E_{OSS}) vs. drain-to-source voltage (V_{DS})

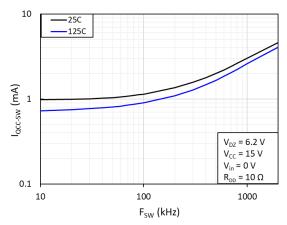


Fig.12. V_{CC} operating current (I_{QCC-SW}) vs. operating frequency (F_{SW})

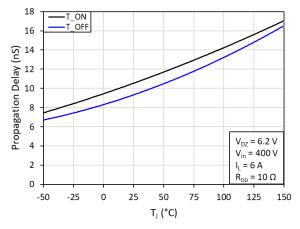


Fig.14. Propagation delay $(T_{ON} \text{ and } T_{OFF})$ vs. junction temperature (T_{J})





Characteristic Graphs (Cont.)

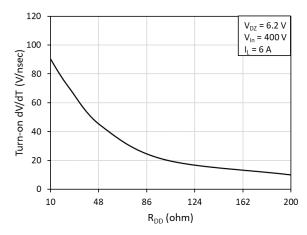


Fig.15. Slew rate (dV/dt) vs. gate drive turn-on current set resistance (R $_{DD}$) at T = 25 $^{\circ}C$

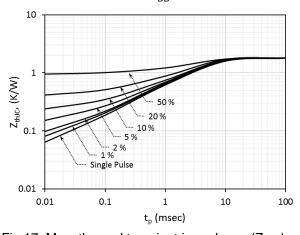


Fig.17. Max. thermal transient impedance (Z_{thJC}) vs. pulse width (t_p)

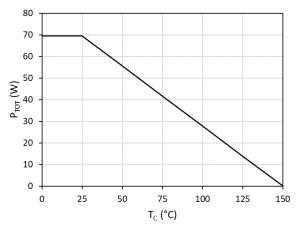
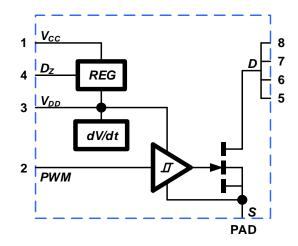


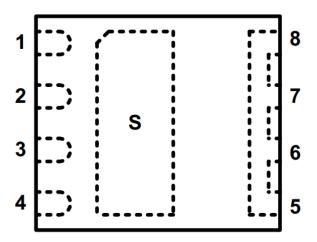
Fig.16. Power dissipation (P_{TOT}) vs. case temperature (T_{C})





7. Internal Schematic, Pin Configurations and Functions





Package Top View

Р	in	I/O ⁽¹⁾	Description	
Number	Symbol	1/0	Description	
1	V _{cc}	Р	Supply voltage (10V to 24V)	
2	PWM	1	PWM input	
3	V _{DD}	I	Gate drive supply voltage. Gate drive turn-on current set pin (using $R_{\tiny DD}$).	
4	D _z	1	Gate drive supply voltage set pin (6.2 V zener to GND).	
5,6,7,8	D	Р	Drain of power FET	
PAD	S	O, G	Source of power FET & GaN IC supply ground. Metal pad on bottom of package.	

(1) I = Input, O = Output, P = Power, G = GaN IC Ground

Final Datasheet 10 Rev 6-4-2018





8. Functional Description

The following functional description contains additional information regarding the IC operating modes and pin functionality.

8.1. Start Up

When the V_{CC} supply is first applied to the NV6117, care should be taken such that the V_{DD} and D_Z pins are up at their correct voltage levels before the PWM input signal starts. The V_{DD} pin ramp up time is determined by the internal regulator current at this pin and the external C_{VDD} capacitor. Also, since the D_Z pin voltage sets the V_{DD} voltage level, the V_{DD} pin will ramp up together with the D_Z pin (Fig.18).

For half-bridge configurations, it is important that the V $_{\rm CC}$ supply, the D $_{\rm Z}$ pin, and the V $_{\rm DD}$ supply of the high-side NV6117 are all charged up to their proper levels before the first high-side PWM pulses start. For LLC applications, a long on-time PWM pulse to the low-side (> 10 μ s) is typically provided by the LLC controller to allow the supply pins of the high-side NV6117 to charge up (through the external bootstrap diode) to their correct levels before the first high-side PWM pulses start (Fig.19).

For active clamp flyback (ACF) applications, the half-bridge must be ready very quickly due to the soft-start mode of the ACF controller. When the first few PWM pulses are generated by the ACF controller, the high-side supply pins of the NV6117 will require a few low-side pulses to charge up (through the external bootstrap diode) before the high-side starts to switch (Fig.20).

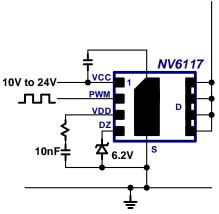


Fig.18. Quick start-up circuit

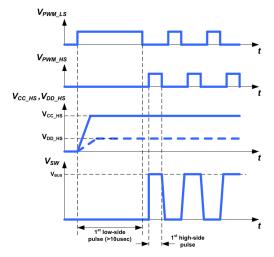


Fig.19. LLC half-bridge start-up timing diagram

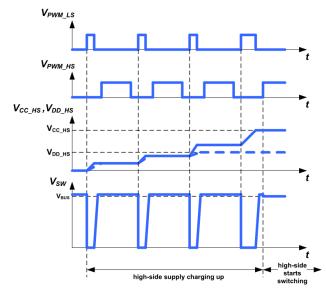


Fig.20. ACF half-bridge start-up timing diagram





8.2. Normal Operating Mode

During Normal Operating Mode, all of the internal circuit blocks are active. V_{CC} is operating within the recommended range of 10 V to 24 V, the V_{DD} pin is at the voltage set by the zener diode at the D_Z pin (6.2 V), and the internal gate drive and power FET are both enabled. The external PWM signal at the PWM pin determines the frequency and duty-cycle of the internal gate of the power FET. As the PWM voltage toggles above and below the rising and falling input thresholds (4 V and 1 V), the internal gate of the power FET toggles on and off between V_{DD} and 0 V (Fig.21). The drain of the power FET then toggles between the source voltage (typically power ground) and a higher voltage level (650 V max), depending on the external power conversion circuit topology.

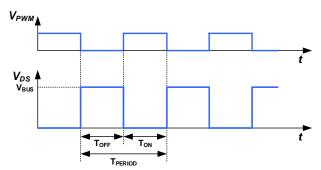


Fig.21. Normal operating mode timing diagram

8.3. Standby Mode

For applications where a low standby power is required, an external series cut-off circuit (Fig.22) can be used to disconnect $V_{\rm CC}$ of the NV6117 from the main $V_{\rm CC}$ supply of the power supply. This will reduce $V_{\rm CC}$ current consumption when the converter is in burst mode during light-load or open load conditions. The $V_{\rm CC}$ cut-off circuit consists of a series PMOS FET that is turned on and off with a pull-down NMOS FET. The gate of the NMOS is controlled by an external ENABLE signal that should be provided by the main controller of the power supply. The capacitor value at the $V_{\rm CC}$ pin should then be selected according to the desired start-up speed of the NV6117 each time the ENABLE signal toggles high. A 22 nF capacitor at $V_{\rm CC}$, for example, will give a typical start-up time of approximately 2 μs .

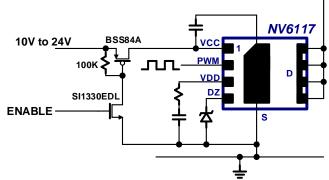


Fig.22. Standby mode Vcc cut-off circuit

8.4. Programmable Turn-on dV/dt Control

During first start-up pulses or during hard-switching conditions, it is desirable to limit the slew rate (dV/dt) of the drain of the power FET during turn-on. This is necessary to reduce EMI or reduce circuit switching noise. To program the turn-on dV/dt rate of the internal power FET, a resistor (R $_{\rm DD}$) is placed in between the V $_{\rm DD}$ capacitor and the V $_{\rm DD}$ pin. This resistor (R $_{\rm DD}$) sets the turn-on current of the internal gate driver and therefore sets the turn-on falling edge dV/dt rate of the drain of the power FET (Fig.23). A typical turn-on slew-rate change with respect to R $_{\rm DD}$ is shown in Fig.15.

Minimum 10 Ω R_{DD} is required.

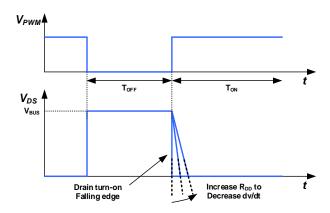


Fig.23. Turn-on dV/dt slew rate control





8.5. Current Sensing

For many applications it is necessary to sense the cycle-by-cycle current flowing through the power FET. To sense the current flowing through the NV6117, a standard current-sensing resistor can be placed in between the source and power ground (Fig.24). In this configuration, all of the components around the NV6117 (C_{VCC} , C_{VDD} , D_{z} , etc.) should be grounded with a single connection at the source. Also, an additional RC filter can be inserted between the PWM signal and the PWM pin (100 Ω , 100 pF typical). This filter is necessary to prevent false triggering due to high-frequency voltage spikes occurring at the source node due to external parasitic inductance from the source PCB trace or the current-sensing resistor itself.

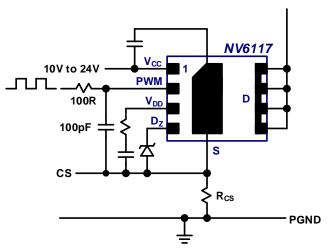


Fig.24. Current sensing circuit

8.6. Paralleling Devices

For some applications it is desirable to parallel ICs in order to reduce conduction losses and temperatures. Two NV6117 ICs can be connected in parallel in a PFC boost application working in boundary-conduction mode (BCM) only. The parallel configuration for two NV6117 ICs is shown in Fig.25. The paired pins that are connected together include the drain pins (D), the source pins (S), the V_{CC} pins, the PWM pins, and the D_Z . A single D_7 diode can be shared by both ICs. The V_{DD} pins are not connected together and require separate V_{DD} supply capacitors (C_{VDD1} , C_{VDD2}) and separate turnon current set resistors (RDD1, RDD2). Each IC should have its own local V_{CC} supply filter capacitor (C_{VCC1} , C_{VCC2}). The PWM pins can have a single filter resistor $(R_{\tiny PWM})$ but separate filter capacitors $(C_{\tiny PWM1},~C_{\tiny PWM2})$ should be placed at the PWM pin of each IC. When designing the PCB layout for the two paralleled ICs, the drain and source connections should be made as symmetrical as possible two avoid any parasitic inductance or capacitance mismatch. A proper PCB layout example for paralleling is shown in Section 11.

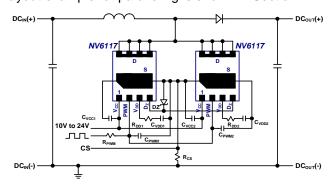


Fig.25. Boost schematic using two parallel ICs





8.7. 3.3V PWM Input Circuit

For some applications where a 3.3 V PWM signal is required (DSP, MCU, etc.) an additional buffer can be placed before the PWM input pin (Fig.26) with the buffer supply voltage connected to the V_{DD} capacitor.

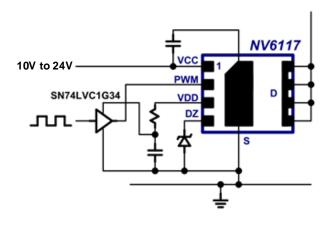


Fig.26. 3.3 V PWM input buffer circuit

8.8. PCB Layout Guidelines

The design of the PCB layout is critical for good noise immunity, sufficient thermal management, and proper operation of the IC. Typical PCB layout examples for without current sensing resistor, with current sensing resistor, and paralleling, are all shown in Sections 10 and 11.

The following rules should be followed carefully during the design of the PCB layout:

- Place all IC filter and programming components directly next to the IC. These components include (C_{VCC}, C_{VDD}, R_{PWM}, C_{PWM}, R_{DD} and D_Z).
- 2) Keep ground trace of IC filter and programming components separate from power GND trace. Do not run power GND currents through ground trace of filter components!
- 3) For best thermal management, place thermal vias in the source pad area to conduct the heat out through the bottom of the package and through the PCB board to other layers (see Sections 10 and 11 for correct layout examples).
- 4) Use large PCB thermal planes (connected with thermal vias to the source pad) and additional PCB layers to reduce IC temperatures as much as possible (see Sections 10 and 11 for correct layout examples).
- 5) For half-bridge layouts, do not extend copper planes from one IC across the components or pads of the other IC!
- 6) For high density designs, use a 4-layer PCB and 2 oz. copper to route signal connections. This allows layout to maintain large thermal copper planes and reduce power device temperature.





8.9. Recommended Component Values

The following table (Table I) shows the recommended component values for the external filter capacitors, zener diode, and R_{DD} connected to the pins of the NV6117. These components should be placed as close as possible to the IC. Please see PCB Layout guidelines for more information. The zener diode at the D_Z pin should be a low-current type with a flat zener, and the min/max limits must be followed. R_{DD} must be a minimum of 10 Ω to ensure application and device robustness.

SYM	DESCRIPTION	PART NO.	SUPPLIER	MIN	TYP	MAX	UNITS
C_{VCC}	Maximum V _{CC} supply capacitor				0.1		μF
$C_{_{VDD}}$	V _{DD} supply capacitor				0.01		μF
$R_{_{DD}}$	Gate drive turn-on current set resistor			10	25	200	Ω
D _z	V _{DD} set zener diode (D _z pin)	BZT52B6V2 RHG	Taiwan Semiconductor Corporation	5.8	6.2	6.6	V
		MM3Z6V2ST1G	ON-Semiconductor				
$R_{_{PWM}}$	PWM filter resistor				100		Ω
C _{PWM}	PWM filter capacitor				100		pF

Table I. Recommended component values.

8.9.1. Zener Selection

The zener voltage is a critical parameter that sets the internal reference for gate drive voltage and other circuitry. The zener diode needs to be selected such that the voltage on the D_Z pin is within recommended operating conditions (5.8 V to 6.6 V) across operating temperature (-40°C to 125°C) and bias current (10 μ A to 1 mA). To ensure effective operation, the current vs. voltage characteristics of the zener diode should be measured down to 10 μ A to ensure flat characteristics across the current operating range (10 μ A to 1 mA). The recommended part numbers meet these requirements. If the zener selected by user does not ensure that the voltage on the zener pin is always within the recommended operating range, the functionality and reliability of the NV6117 can be impacted. An external resistor (~47 k Ω) between V_{CC} and D_Z can improve zener voltage stability by adding bias current to the zener pin to ensure the voltage on the D_Z pin is always within the recommended operating range (Error! Reference source not found.). This will add ~200 μ A of quiescent current.

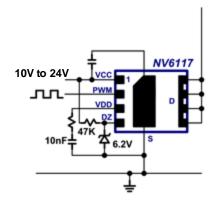
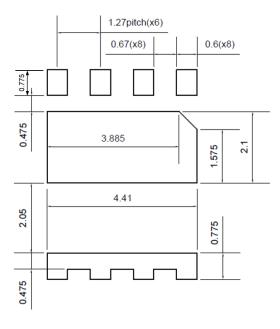


Fig.27. Increasing Zener Bias Current for Stable Zener Voltage

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9. Recommended PCB Land Pattern

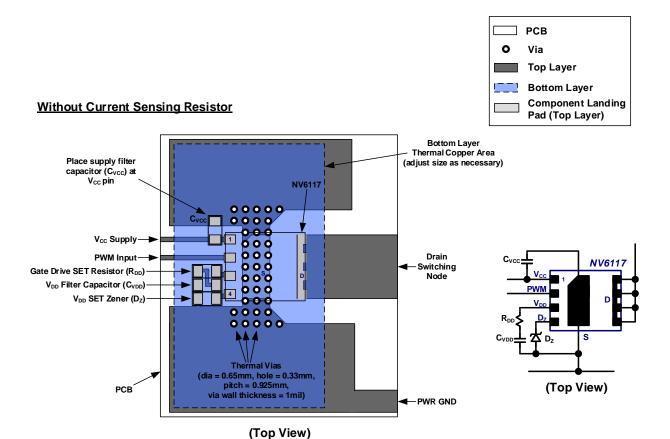


All dimensions are in mm

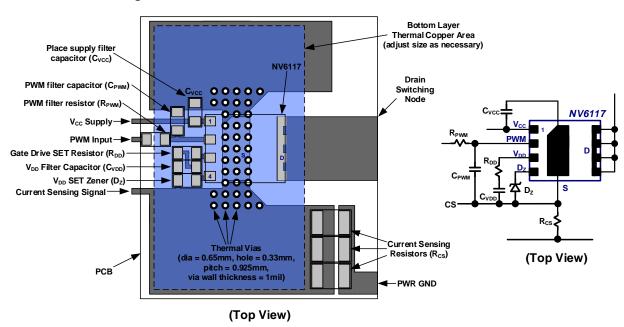




10. PCB Layout Guidelines

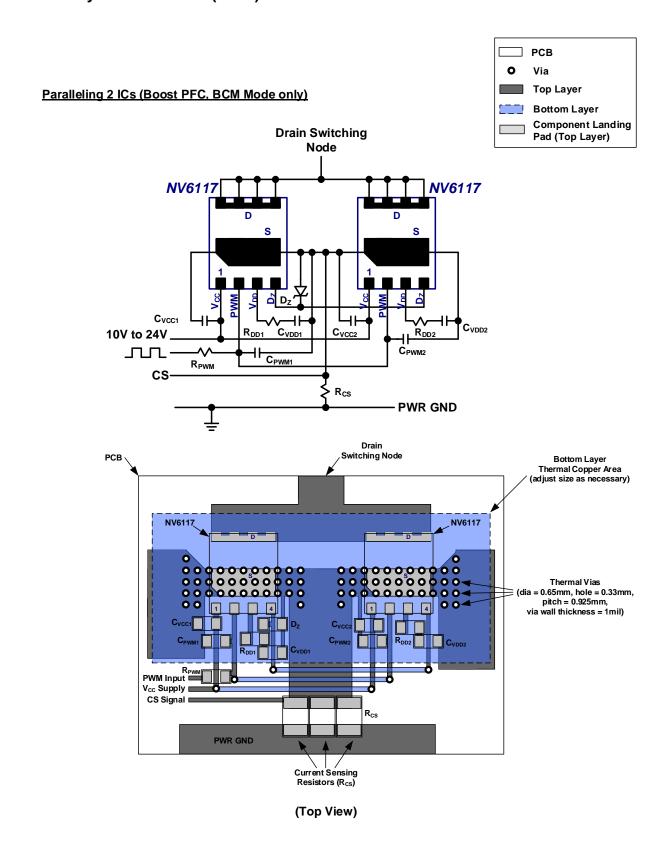


With Current Sensing Resistor



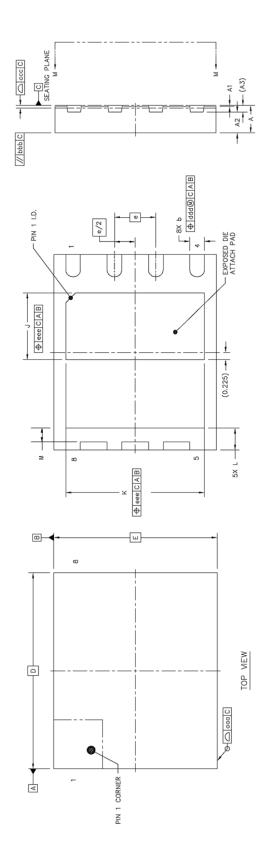


11. PCB Layout Guidelines (cont.)





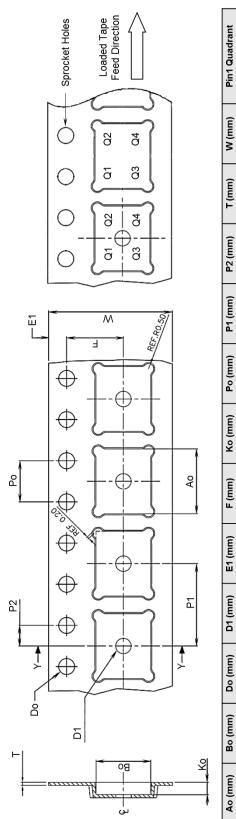
12. QFN Package Outline

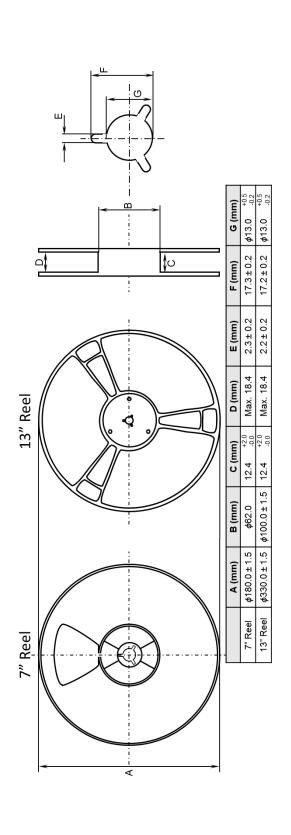


		SYMBOL	MIN	MOM	MAX			SYMBOL	MIN	MOM	MAX
TOTAL THICKNESS		A	0.8	0.85	6.0	CD 617E	×	_	1.95	2.05	2.15
STAND OFF		A1	0	0.035	0.05	בו אולב	\	¥	4.16	4.26	4.36
MOLD THICKNESS		A3	1	0.65	+	LEAD LENGTH		7	0.625	0.675	0.725
L/F THICKNESS		A3		0.203 REF		MERGED LEAD LENGTH	픈	Σ		0.43	
LEAD WIDTH		В	0.4	0.45	0.5	PACKAGE EDGE TOLERANCE	RANCE	aaa		0.1	
BODV 617E	×	٥		6 BSC		MOLD FLATNESS		qqq		0.1	
DODI SIZE	Υ	ш		5 BSC		COPLANARITY		ວວວ		0.08	
LEAD PITCH		Ð		1.27 BSC		LEAD OFFSET		ppp		0.1	
						EXPOSED PAD OFFSET		eee		0.1	



13. Tape and Reel Dimensions





g

 12.00 ± 0.1

 0.30 ± 0.05

 2.0 ± 0.1

 8.00 ± 0.1

 4.0 ± 0.1

 1.20 ± 0.1

 5.50 ± 0.1

 1.75 ± 0.1

min. \$1.50

 $\phi 1.55 \pm 0.05$

 5.30 ± 0.1

6.30 ± 0.1





14. Ordering Information

Part Number	Operating Temperature Grade	Storage Temperature Range	Package	MSL Rating	Packing (Tape & Reel)
NV6117	-40 °C to +125 °C T _{CASE}	-55 °C to +150 °C T _{CASE}	5 x 6 mm QFN	3	1,000 : 7" Reel 5,000 : 13" Reel

Additional Information

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